Intermodulation in nonlinear SQUID metamaterials: Experiment and theory

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The response of nonlinear metamaterials and superconducting electronics to two-tone excitation is critical for understanding their use as low-noise amplifiers and tunable filters. A new setting for such studies is that of metamaterials made of radio frequency superconducting quantum interference devices (rf-SQUIDs). The two-tone response of self-resonant rf-SQUID meta-atoms and metamaterials is studied here via intermodulation (IM) measurement over a broad range of tone frequencies and tone powers. A sharp onset followed by a surprising strongly suppressed IM region near the resonance is observed. Using a two time scale analysis technique, we present an analytical theory that successfully explains our experimental observations. The theory predicts that the IM can be manipulated with tone power, center frequency, frequency difference between the two tones, and temperature. This quantitative understanding potentially allows for the design of rf-SQUID metamaterials with either very low or very high IM response.

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I. INTRODUCTION

Nonlinearity is a key consideration in a wide range of important applications including amplifiers [1-3] and tunable filters [4]. Introduction of nonlinearity into metamaterials facilitates tunability, design flexibility, and selfinduced nonlinear responses [5,6], giving rise to developments in metamaterial-based amplifiers [7,8], filters [9–11], and antennas [12–14]. However, as data streams containing multifrequency signals pass through these nonlinear components, they generate intermodulation (IM) products via frequency mixing [15]. The same issue appears in intrinsically nonlinear superconducting electronics. The IM between two input frequencies f_1 and f_2 leads to products at frequencies $pf_1 \pm qf_2$ (p and q are integers), forming side bands and additional noise that could diminish the performance of superconducting devices [4,16-27]. On the other hand, IM generation can be used as a diagnostic to determine various types of defects in superconductors [28-31], to study unconventional superconductors [28,29,31–41], and to amplify microwave signals [2,27,42,43], even at the quantum limit in Josephson parametric amplifiers [1,3] and Josephson metamaterials [7]. Therefore, IM is of mutual research interest in wireless communication, nonlinear metamaterials, as well as in quantum information processing, and superconducting electronics and materials. Extensive measurement and theory have been devoted to IM in these fields [18,25,44–52].

rf-SQUID metamaterials combine the advantages of superconducting electronics and nonlinear metamaterials [5,53,54]. An rf-SQUID is the macroscopic quantum version of a split ring resonator (SRR) with the gap capacitance in the SRR replaced by a nonlinear Josephson junction. SQUIDs can be very sensitive to dc and rf magnetic flux, on the scale of the flux quantum $\Phi_0 = h/2e = 2.07 \times 10^{-15}$ T m², where *h* is Planck's constant and *e* is the elementary charge. Previous work reveals that rf-SQUID meta-atoms and metamaterials have a resonant frequency tunability of up to 80 THz/G by varying the dc magnetic flux when the driving rf flux amplitude is low [55–57]. In Ref. [58] the authors studied the bistability of rf-SQUID meta-atoms and metamaterials driven by intermediate rf flux amplitudes. The bistability results in a lower resonant frequency and a nearly full disappearance of resonance absorption (transparency). Such broadband transparency can be switched on and off via drive frequency, signal amplitude, or dc flux hysteresis [58]. These properties make rf-SQUID metamaterials attractive for tunable filters, gain-modulated antennas [59], and wideband power limiters for direct-digitizing rf receivers [60] in nextgeneration wireless communication systems.

Basically, an rf-SQUID is a nonlinear resonator with a manipulatable resonant frequency and absorption that depend on the dc and rf flux amplitudes, the temperature, and the drive signal history [55–58,61–69]. We will study IM generation around this tunable, bistable resonance.

In this paper we report comprehensive results from experimental and theoretical IM studies of rf-SQUID meta-atoms and metamaterials around resonance. We focus on the case where two input signals have the same amplitude, as opposed to IM amplification experiments where one tone is much stronger than the other. We find that under certain combinations of tone power and frequency, the SQUID shows a sudden onset of the third order IM generation followed by a near-zero third order IM generation (gap). This phenomenon is a result of the bistable properties of rf-SQUIDs. This intrinsic suppression of IM generation may be useful as a mechanism for depressing signal mixing in communication applications. A detailed theoretical model is presented to explain this surprising gap feature in IM generation. The intensity of IM generation sensitively depends on the parameters of the rf-SQUIDs, and can be modulated by dc/rf magnetic field, and temperature, potentially allowing one to design and tune the IM generation to meet various requirements for applications.

II. EXPERIMENT DETAILS

Two-dimensional metamaterials were constructed by positioning rf-SQUID meta-atoms in a square grid array on a planar substrate [Fig. 1(a)]. The single rf-SQUID



FIG. 1. (a) Left: The optical image of meta-atoms of a 27×27 array metamaterial. Inset shows details of a single SQUID. Right: The 3D structure of a single rf-SQUID. The distance between two niobium layers is exaggerated to show the overlap capacitance. (b) The experimental setup for our IM measurements. (c) The circuit model for a single SQUID. (d) Experimental measurements of output power from the 27×27 rf-SQUID metamaterial at a temperature of T = 4.6 K as a function of frequency when two signals of the same amplitude are injected at a center frequency of 21.499 GHz and a difference frequency of 1 MHz.

meta-atoms, and the metamaterials, were fabricated using the Hypres 0.3 $\mu A/\mu m^2 Nb/AlO_x/Nb$ junction process on silicon substrates, and the meta-atom has a superconducting transition temperature $T_c = 9.2$ K. A 3D perspective drawing of a single rf-SQUID is shown in Fig. 1(a). Two Nb films (135 and 300 nm thick) connected by a via and a Josephson junction make up the superconducting loop with geometrical inductance L. The capacitance C has two parts: the overlap between two layers of Nb with 200 nm thick SiO₂ dielectric in between, and the Josephson junction intrinsic capacitance. A single rf-SQUID can thus be treated as a resistively and capacitively shunted Josephson junction (RCSJ model) in parallel with superconducting loop inductance [Fig. 1(c)]. The rf-SQUIDs are designed to be low noise $\{\Gamma = 2\pi k_B T / (\Phi_0 I_c) < 1, \text{ where } T \text{ is the temperature, } I_c \text{ is } \}$ the critical current in the Josephson junction, $\Phi_0 = h/2e$ is the

quantum flux, and $L_F = (k_B T)^{-1} [\Phi_0/(2\pi)]^2 \gg L$ [70]} and nonhysteretic ($\beta_{\rm rf} = 2\pi L I_c/\Phi_0 < 1$). No dc magnetic flux is applied for this set of experiments.

In the experimental setup Fig. 1(b), the rf-SQUID array sits in a rectangular waveguide orientated so that the rf magnetic field of the TE mode is perpendicular to the rf-SQUIDs. Before each two-tone experiment, a single-tone transmission experiment is conducted to determine the resonant frequency at which the system has maximum power absorption. IM products are then measured systematically around the resonance; two signals of frequencies f_1 and f_2 having the same amplitude and a small difference in frequency $\Delta f = f_2 - f_1 > 0$ are injected. The output signal contains the two main tones and their harmonics, as well as IM products.

An example of the generation of an IM spectrum in the metamaterial around resonance (of a 27×27 array of rf-SQUIDs) is shown in Fig. 1(d) with $\Delta f = 1$ MHz. This spectrum was measured under a fixed tone center frequency and a fixed tone power. The output signal at frequency $f_i = pf_1 + qf_2$ is called the (|p| + |q|)th order IM. We focus on nearby IM products which are of the third, fifth, seventh,... order. The IM signals generated at nearby frequencies $f_3 = 2f_1 - f_2$ and $f_4 = 2f_2 - f_1$, called the lower and upper third order IM $(f_2 > f_1)$, respectively, are of most concern in communications and mixing applications. When the metamaterial is superconducting (measured at T = 4.6 K), there is strong IM generation observed above the noise floor up to 51st order. There is no observed IM output when temperature is above the transition temperature $T_c = 9.2 \text{ K}.$

The IM spectrum changes considerably as the center frequency and tone power are varied. We mainly examine the modulation of the third order IM power. Again we first search for resonance in a single-tone experiment as the input power varies. In the intermediate power regime, higher input power results in a shift of the resonant frequency to lower values [58], as seen in the purple curve in Fig. 2(a). The third order IM power is then measured with two-tone input around the resonance. Figure 2(a) shows the upper third order IM power P_{f_4} (colors) generated from a single rf-SQUID meta-atom as a function of the input tone power (horizontal axis) and the center frequency (vertical axis) of the two tones. The IM generation generally follows the resonant frequency curve. Intermodulation is small for low input tone powers (< -80 dBm), with a peak just below the resonant frequency. As the input power increases, the IM generation also increases while shifting to lower frequencies. At the same time a second peak appears above the resonant frequency, forming an IM gap where the IM is reduced to nearly the noise level around the resonant frequency. The same phenomenon is observed for a 7×7 array rf-SQUID metamaterial and an 11×11 array rf-SQUID metamaterial. Operating the meta-atom or metamaterial in the gap regime minimizes the third order IM frequency mixing.

Figure 2(c) compares the measured lower and upper third order IM products (P_{f_3} and P_{f_4}) as a function of frequency around the gap feature at -65 dBm. Both IM powers show a sharp onset above the noise level at around 17 GHz, and decrease to a minimum value at 18 GHz, then reach another peak at around 18.4 GHz before dropping continuously at



FIG. 2. The upper third IM power P_{f_4} generated from a single rf-SQUID meta-atom as a function of the applied rf flux and the center frequency of the two tones for (a) experiment and (b) numerical simulation. The purple curve indicates the resonant frequency for a single-tone excitation. The frequency cut for output power at the third IM P_{f_3} (blue solid line) and P_{f_4} (black dashed line) at -65 dBm for (c) experiment and (d) simulation. Note that (c) is plotted by averaging the measured frequency cut at the tone power ranging from -65.2 to -64.8 dBm (with a step of 0.1 dBm) to reduce the noise. The spacing between the two input tones is 10 MHz, and the temperature is 4.6 K.

higher frequencies. However, the upper tone P_{f_4} has a higher peak and a substantially lower dip than the lower tone P_{f_3} . This asymmetry between two same-order IM tones was also observed in other SQUID samples and in our numerical simulations. We now wish to explore the origins of the features seen in the data, including the sharp onset and the dip in the third IM generation, as well as the asymmetry between the upper and lower IM output signals.

III. MODELING

A. Numerical simulation

In this section we explore a simple circuit model that reproduces the effects seen in the previous sections. The circuit model suggests treating a single rf-SQUID as an RCSJ in parallel with superconducting loop inductance [Fig. 1(c)]. We assume a uniformly driven and uncoupled SQUID array metamaterial can also be described by the single junction RCSJ model. The macroscopic quantum gauge-invariant phase difference across the junction δ determines the current through the junction $I = I_c \sin \delta$ (I_c is the critical current of the junction). In a closed superconducting loop δ is related to the total magnetic flux inside the loop: $\delta - 2\pi \Phi_{tot}/\Phi_0 = 2\pi n$, where *n* is an integer, and again $\Phi_0 = h/2e$. Here we can take *n* to be 0 without loss of generality as shifting δ by 2π leaves the current *I* unchanged [71]. The voltage across the junction can be written as $V = 2\pi \Phi_0 d\delta/dt$.

The time evolution of the phases is determined by the RCSJ circuit equation [71], obtained by demanding that the total flux through the loop Φ_{tot} is the combination of the dc and rf applied flux $[\Phi_{dc} + \Phi_{rf}(t)]$, and the induced flux due to the self inductance *L* of the loop,

$$\Phi_{\rm tot} = \Phi_{\rm dc} + \Phi_{\rm rf}(t) - L \left(I_c \sin \delta + \frac{V}{R} + C \frac{dV}{dt} \right).$$
(1)

Here $I_c \sin \delta + V/R + CdV/dt$ is the total current through the loop, which flows through the parallel combination of the junction, shunt resistance *R*, and capacitance *C* in the RCSJ model. Replacing Φ_{tot} by $\Phi_0 \delta/2\pi$ and *V* by $\Phi_0 d\delta/dt$ in Eq. (1) and rearranging terms, we obtain the dimensionless RCSJ equation:

$$\frac{d^2\delta}{d\tau^2} + \frac{1}{Q}\frac{d\delta}{d\tau} + \delta + \beta_{rf}\sin\delta = \phi_{\rm dc} + \phi_{\rm rf}(\tau), \qquad (2)$$

where $\beta_{\rm rf} = 2\pi L I_c / \Phi_0$, $\phi_{\rm dc} = 2\pi \Phi_{\rm dc} / \Phi_0$, $\phi_{\rm rf} = 2\pi \Phi_{\rm rf} / \Phi_0$, $\omega_{\rm geo} = (LC)^{-1/2}$, $\tau = \omega_{\rm geo} t$, and $Q = R \sqrt{C/L}$.

Typical parameter values are as follows. The inductance, L = 280 pH, of the single SQUID meta-atom is calculated numerically by Fasthenry based on its geometrical structure [72]. Other parameters such as the capacitance C = 0.495 pF, the shunt resistance in the junction R = 1780Ohm (4.6 K), and the critical current $I_c = 1.15 \ \mu A$, are determined by fitting to the measured geometrical resonant frequency $\omega_{\rm geo}/2\pi = 13.52$ GHz, the measured quality factor Q = 75, and the quantity $\beta_{\rm rf} = 0.98$. The quantities $\omega_{\rm geo}$, Q, and $\beta_{\rm rf}$ were directly measured in previous single-tone transmission experiments [57,58]. For our setup, the rf flux $\phi_{\rm rf}$ driving the loop results from the injected rf power inside the rectangular waveguide. Note that the single SQUID meta-atom has an inner diameter of 200 μ m, and an outer diameter of 800 μ m. Other meta-atoms in our SQUID metamaterials all have smaller sizes. Thus the rf flux amplitude through the SQUID loop is always much smaller than the flux quantum in the rf power range we consider in this work. Thus, $|\phi_{\rm rf}| < 2\pi$.

The time-dependent functional form of the rf flux is determined by the driving signal. To study intermodulation, the circuit is driven with two tones, which generally can be written

$$\phi_{\rm rf} = \phi_{\rm rf,1} \sin(\Omega_1 \tau + \theta_1) + \phi_{\rm rf,2} \sin(\Omega_2 \tau + \theta_2), \quad (3)$$

where $\Omega_{1,2} = 2\pi f_{1,2}/\omega_{\text{geo}}$ and f_1 and f_2 are the frequencies of the two injected signals. Here the two tones have different amplitudes $\phi_{\text{rf},1}$ and $\phi_{\text{rf},2}$, and phases θ_1 and θ_2 .

The driving flux can also be written in the form of a complex phasor envelope modulated by a carrier at the mean frequency $\Omega = (\Omega_1 + \Omega_2)/2$,

$$\phi_{\mathrm{rf},a} = \mathrm{Re}[e^{i\Omega\tau - i\pi/2}\phi_e(\tau)],\tag{4}$$

where the envelope function $\phi_e(\tau) = \phi_{\text{rf},1} \exp(-i\Delta\Omega\tau/2 + i\theta_1) + \phi_{\text{rf},2} \exp(i\Delta\Omega\tau/2 + i\theta_2)$ and $\Delta\Omega = \Omega_2 - \Omega_1 > 0$ is the difference frequency. For the situation in our experiment, $\Delta\Omega \ll \Omega$, i.e., the carrier frequency is much greater than the envelope frequency. This will lead to a number of simplifications in the analysis. At present it allows us to argue



FIG. 3. The lower and higher main tone output amplitudes δ_1 and δ_2 , and third order tones δ_3 and δ_4 for a single rf-SQUID meta-atom at -65 dBm calculated with (a) numerical simulation and (b) analytical model. Plots of $\delta(t)$ over a beat period at 17.35 GHz and -65 dBm calculated by (c) numerical simulation and (d) steady-state analytical model. The dashed boxes in (c) point out the overshooting ringing features in numerical simulation. The spacing between the two input tones is 10 MHz, the temperature is 4.6 K, and the applied dc flux is set to zero.

that the results will not depend on the relationship between the carrier and the envelope phases. Since the relative phase between the carrier and the envelope is unimportant we may shift the time axis in the carrier and the envelope independently. Shifting time in the carrier by $\tau_{sc} = -\Omega^{-1}(\theta_1 + \theta_2)$ and in the envelope by $\tau_{se} = \Delta \Omega^{-1}(\theta_1 - \theta_2)$ removes the phases θ_1 and θ_2 from the problem. Equivalently we can set $\theta_1 = \theta_2 = 0$.

We first consider the case of equal amplitude tones (set $\phi_{\rm rf,1} = \phi_{\rm rf,2} = \phi_s$ to be the amplitude) and set $\theta_1 = \theta_2 = 0$. We then solve Eq. (2) for $\delta(\tau)$ using the previously described circuit parameters. Under all circumstances explored here $\delta(\tau)$ is observed to be sinusoidal to a good approximation. Figure 3(c) is an example of the solution to $\delta(\tau)$ at an input power of -65 dBm, with tone frequencies f_1 and f_2 centered around f = 17.35 GHz and separated by of $\Delta f = 10$ MHz. The dense blue curves are the fast carrier oscillations and the vertical extreme of the blue represents the slowly varying envelope. More precisely, $\delta(\tau)$ can be represented in the form of a modulated complex phasor envelope, the same as the form of the driving rf flux in Eq. (4). In this example, the envelope varies on a time scale 3 orders of magnitude longer than the carrier period. One beat period of the envelope is shown in Fig. 3(c).

Furthermore, to investigate IM, we extract the amplitude and phase of δ_i for frequency component f_i via Fourier transform of $\delta(\tau)$. Since magnetic flux is related to δ through $\delta = 2\pi (\Phi_{tot}/\Phi_0)$, we can extract the generated third order IM magnetic flux $\Phi_{3,4}$. The IM flux translates into an IM magnetic field inside the SQUID loop of area A, i.e., $B_{3,4} = \Phi_{3,4}/A$. The excited IM magnetic field transmits through the rectangular waveguide and generates the third order IM powers at the detector. The SQUID is inductively coupled to the waveguide via a coupling coefficient g [73], so only part of the IM power couples to the waveguide mode. The final simulated output IM power is adjusted by varying g ($g \approx 0.015$ for the single SQUID meta-atom), and plotted as a function of center frequency and tone power in Fig. 2(b) for the upper third order IM tone P_{f_4} , with a cut through -65 dBm plotting both lower and upper third order IM powers (P_{f_3} and P_{f_4}) in Fig. 2(d). The cut through the simulated IM power displays a similar sharp onset and gap feature as observed in the experiment, as well as the prominent asymmetry between the two IM tones.

Since δ_i is a surrogate for the output tone power P_{f_i} $(\delta_i \sim \sqrt{P_{f_i}})$ and a direct solution of the nonlinear equation, we use this quantity to analyze the degree of IM generation. Figure 3(a) shows amplitudes of δ_1 to δ_4 as a function of tone center frequency at an input power of -65 dBm, which shows the same asymmetric gap feature. The upper third order IM output δ_4 reduces to nearly zero inside the gap. We plot $\delta(t)$ during one beat period of the input rf signal at the onset center frequency (17.35 GHz) of the abrupt IM generation peak in Fig. 3(c). The $\delta(t)$ envelope stays at a higher amplitude in the first quarter of the signal beat period, suddenly decreases to a low amplitude, and gradually increases before it jumps to a higher amplitude again. Note that each abrupt jumps comes with an overshoot feature [labeled as dashed boxes in Fig. 3(c)] with a frequency around 1.5 GHz. The overshoot frequency is intermediate to the fast oscillation (17.35 GHz) and the slow modulations (10 MHz).

B. Steady-state analytical model

In this section we develop an analytical model to understand the unique phenomena revealed in the experiment and the numerical solutions of the previous sections. We adopt the observation that the gauge-invariant phase $\delta(\tau)$ and the driving flux can be represented as in Eq. (4) as a rapidly varying carrier modulated by an envelope. Thus, we insert Eq. (4) on the right-hand side of Eq. (2). We first look for solutions where the time variation of the envelope is so slow that the temporal derivatives of it can be ignored. This leads (after neglecting harmonics of the drive signal, which will be justified below) to a time dependent gauge-invariant phase:

$$\delta(\tau) = \bar{\delta} + \tilde{\delta}\sin(\Omega\tau + \theta),$$

where $\Omega = (\omega_1 + \omega_2)/(2\omega_{geo})$ and $\bar{\delta}$, $\bar{\delta}$, and θ are taken to be constants that depend parametrically on τ through the slow variation of $\phi_{rf}(\tau) = \tilde{\phi}_{rf} = \phi_e$. Here $\bar{\delta}$ and $\tilde{\delta}$ denote the dc part and the slowly varying envelope of δ , respectively, θ is the phase of δ (which can also vary slowly with time).

For the nonlinear term in Eq. (2) we have $\sin \delta = \sin[\bar{\delta} + \tilde{\delta} \sin(\Omega \tau + \theta)] = \sin \bar{\delta} \cos[\tilde{\delta} \sin(\Omega \tau + \theta)] + \cos \bar{\delta} \sin[\tilde{\delta} \sin(\Omega \tau + \theta)]$. In principle this term will contain all harmonics of the carrier, $n\Omega$ (n = 0, 1, 2, ...), and induce harmonics in the gauge-invariant phase $\delta(\tau)$. However, higher harmonics in the gauge-invariant phase are suppressed by the second derivative term in Eq. (2) (capacitive current). This is confirmed in our numerical solutions where the amplitudes of higher harmonics (components of frequency 2Ω and 3Ω) of δ are at least 2 orders of magnitude lower than the fundamental frequency component. We note that for the examples considered here the dc phase $\bar{\delta}$ is zero and consequently only odd harmonics are present. We thus neglect these higher order harmonic terms when we expand $\sin[\tilde{\delta} \sin(\Omega\tau + \theta)]$ and $\cos[\tilde{\delta} \sin(\Omega\tau + \theta)]$. As a result, we



FIG. 4. Analytical solutions of steady-state model [Eqs. (5)–(7)] at an rf power of -65 dBm which is around the gap feature. (a) The relationship between $\tilde{\delta}$ and $\tilde{\phi}_{rf}$ for five remarkable frequencies. ϕ_{lh} denotes the value of rf flux required for transitions of $\tilde{\delta}$ from low to high amplitude solution branch, and ϕ_{hl} denotes the rf flux value for the transition from high to low amplitude solution. (b)–(f) Blue curves represent $\delta(t)$ calculated by the analytical model for (a) 17.3 GHz, right before the onset of strong IM generation, (b) 17.35 GHz, at the onset, (c) 17.7 GHz, at the gap, (d) 18.4 GHz, at the second peak, and (e) 19.5 GHz, low IM generation. The red curve is $\tilde{\phi}_{rf}$ as a function of time during a beat period. ϕ_{lh} and ϕ_{hl} are marked in the figures as black and green lines. All assume $\phi_{dc} = 0$.

obtain $\sin \delta \approx \sin \bar{\delta} J_0(\tilde{\delta}) + 2 \cos \bar{\delta} J_1(\tilde{\delta}) \sin(\Omega \tau + \theta)$, where $J_0(\tilde{\delta})$ and $J_1(\tilde{\delta})$ are Bessel functions. Separating the dc, in-phase, and quadrature components of Eq. (2), leads to three coupled equations for the three unknowns $(\bar{\delta}, \tilde{\delta}, \text{ and } \theta)$,

$$(1 - \Omega^2)\tilde{\delta} + 2\beta_{\rm rf}\cos\bar{\delta}J_1(\tilde{\delta}) = \tilde{\phi}_{\rm rf}\cos\theta, \qquad (5)$$

$$\frac{\Omega}{Q}\tilde{\delta} = -\tilde{\phi}_{\rm rf}\sin\theta,\tag{6}$$

$$\bar{\delta} + \beta_{\rm rf} \sin \bar{\delta} J_0(\tilde{\delta}) = \phi_{\rm dc}.$$
(7)

We construct $\delta(t)$ by solving Eqs. (5)–(7) to find $\bar{\delta}$, $\tilde{\delta}$, and θ for a given $\tilde{\phi}_{rf}$ and ϕ_{dc} . The relationship between $\tilde{\delta}$ and $\tilde{\phi}_{rf}$ at different frequencies $(f_1 + f_2)/2$ is plotted in Fig. 4(a) for our standard parameter set $\phi_{dc} = 0$, Q = 75, and $\beta_{rf} = 0.98$. The oscillation amplitude $\tilde{\delta}$ as a function of rf flux amplitude $\tilde{\phi}_{rf}$ is symmetric about the origin, so only positive $\tilde{\phi}_{rf}$ is shown. Figure 4(a) indicates that $\tilde{\delta}$ can be single valued or multivalued depending on the fast-oscillation frequency and the slowly varying envelope amplitude $\tilde{\phi}_{rf}$. For cases where $\tilde{\delta}$ is multivalued, we let ϕ_{hl} and ϕ_{lh} denote the lower and

upper critical rf flux values [as labeled in Fig. 4(a)] between which there are three solutions for the oscillation amplitude $\tilde{\delta}$. When this occurs ($\phi_{hl} < \tilde{\phi}_{rf} < \phi_{lh}$) the middle solution is always unstable and the largest and the smallest solutions are stable. Thus, if $\tilde{\phi}_{rf}$ is in the bistable regime, and $\tilde{\delta}$ is on the lower (higher) stable branch, then, as $\tilde{\phi}_{rf}$ is slowly increased (decreased) through ϕ_{lh} (ϕ_{hl}), the solution for $\tilde{\delta}$ will experience a jump transition from the lower (higher) stable branch to the higher (lower) stable branch.

For two equal amplitude input tones with a fixed center frequency and a fixed tone power $\tilde{\phi}_{rf}$ is a sinusoidal function with a peak value of $2\phi_s$, and a frequency of $\Delta\Omega/2$, i.e. $\tilde{\phi}_{rf} = 2\phi_s \cos \Delta\Omega \tau/2$.

Figures 4(b)-4(f) show the evolution of $\delta(t)$ at different center frequencies (blue), as well as the relationship between the envelopes of the rf flux $\tilde{\phi}_{rf}$ (red curves), the transition rf flux values ϕ_{lh} (black horizontal lines) and ϕ_{hl} (green horizontal lines) for positive and negative $\tilde{\phi}_{rf}$ values during a beat period $(\omega_{geo}\Delta\Omega/2\pi = 10 \text{ MHz})$. For tone center frequencies below 17.3 GHz, although $\tilde{\delta}$ is bistable, the envelope of rf flux $\tilde{\phi}_{rf}$ is always below ϕ_{lh} , so $\tilde{\delta}$ remains on the low amplitude branch during a beat period. Above 18.6 GHz, $\tilde{\delta}$ as a function of $\tilde{\phi}_{rf}$ becomes single valued. Both cases give rise to low IM generation.

Between 17.3 and 18.6 GHz, however, the peak value of $\tilde{\phi}_{rf}$ exceeds the upper bistable transition rf flux amplitude ϕ_{lh} , while the minimum value of $\tilde{\phi}_{rf}$ is below ϕ_{hl} , so there are four discontinuous jumps in $\delta(t)$ during a beat period. Changing the center frequency from 17.35 to 17.7 GHz makes the solutions for $\tilde{\delta}$ stay on the high-amplitude branch longer [Fig. 4(d)]. This is because ϕ_{lh} is smaller for higher frequencies [as seen in Fig. 4(a)], so it is easier for $\tilde{\phi}_{rf}$ to pass the low-to-high transition. The sudden asymmetric state jumps during a beat period generates rich IM products.

We extract the IM components of δ by Fourier transform as discussed for the numerical simulation, and extract the amplitude of two main tones and two third order IM tones of δ , plotted in Fig. 3(b). The analytically calculated amplitudes of IM tones are almost the same as those in the full numerical simulation. However, comparison of time dependent gaugeinvariant phase $\delta(t)$ between the full numerical calculation and the analytical calculation in Figs. 3(c) and 3(d) indicates that the dynamical ringing appears around the state jumps in the full-nonlinear numerical calculation but is not present in the steady-state solutions to Eqs. (5) to (7). These will be investigated subsequently.

C. Dynamical model

The ringing behavior of $\delta(t)$ during state jumps indicates that the system requires time to transition from one stable state to another. We study this process using a dynamical model for the complex amplitude of the phase $\hat{\delta}$, where $\delta(\tau) = \bar{\delta} + \text{Re}[\hat{\delta}(\tau)e^{i\Omega\tau - i\pi/2}]$.

For two equal amplitude input tones, the envelope of the rf flux $\hat{\phi}_{rf} = \phi_e = 2\phi_s \cos(\Delta\Omega\tau/2)$ is real. In this case, sin δ is expanded as $\sin \bar{\delta} J_0(|\hat{\delta}|) + 2\cos \bar{\delta} J_1(|\hat{\delta}|) \operatorname{Re}(\hat{\delta} e^{i\Omega\tau - i\pi/2})/|\hat{\delta}|$ with negligible higher order terms assuming that the higher harmonics of δ are much smaller than the base frequency component. In deriving an equation for the envelope, we adopt

the approximations that $Q \gg 1$ and that $\hat{\delta}(\tau)$ changes slowly, $|\Omega \hat{\delta}| \gg |d\hat{\delta}/d\tau|$. Thus in Eq. (2) we replace $d/(Qd\tau)$ with $i\Omega/Q$, and $d^2/d\tau^2$ with $-\Omega^2 + 2i\Omega d/d\tau$. This yields a first-order nonlinear equation for the phasor $\hat{\delta}$ and a transcendental equation for the steady part of $\delta(t)$,

$$i\Omega\left[2\frac{d}{d\tau} + \frac{1}{Q}\right]\hat{\delta} + \left[1 - \Omega^2 + \beta_{\rm rf}\cos\bar{\delta}\frac{2J_1(|\hat{\delta}|)}{|\hat{\delta}|}\right]\hat{\delta} = \hat{\phi}_{\rm rf},\tag{8}$$

$$\bar{\delta} + \beta_{\rm rf} \sin \bar{\delta} J_0(|\hat{\delta}|) = \phi_{\rm dc}.$$
(9)

To analyze the dynamics, we express $\hat{\delta}$ as an in-phase part and a quadrature part, i.e., $\hat{\delta} = \delta_R + i\delta_I$, and write the real and imaginary parts of Eq. (8). We note that in the absence of losses $(Q \to \infty)$ one can construct a Hamiltonian function for the nonlinear system. Including losses we have

$$\frac{d}{d\tau}\delta_R = -\frac{1}{2Q}\delta_R - \frac{\partial}{\partial\delta_I}H(|\hat{\delta}|), \qquad (10a)$$

$$\frac{d}{d\tau}\delta_I = -\frac{1}{2Q}\delta_I + \frac{\partial}{\partial\delta_R}H(|\hat{\delta}|), \qquad (10b)$$

where

$$H = \frac{1}{4\Omega} [(1 - \Omega^2)|\hat{\delta}|^2] - 2\beta_{\rm rf} \cos \bar{\delta} J_0(|\hat{\delta}|) - \delta_R \hat{\phi}_{\rm rf}$$

is the Hamiltonian. Equilibrium states of the system Eq. (10) are the same as those described by Eqs. (5)–(7). However, we note that the Q value for our system is quite large, $Q \approx 75$. As a result we look for equilibria of the lossless system $Q \rightarrow \infty$, which are located in the δ_R - δ_I plane at the stationary values of the Hamiltonian $\partial H/\partial \delta_R = \partial H/\partial \delta_I = 0$. Equilibria will be stable if they are at maximal or minimal points of H when $(\partial^2 H/\partial \delta_I^2)(\partial^2 H/\partial \delta_R^2) > 0$. Note that the Hamiltonian is symmetric about $\delta_I = 0$.

In Figs. 5(a)-5(c) we plot the Hamiltonian as a function of δ_R and δ_I at a center frequency of 17.35 GHz and -65 dBm tone power, when the rf flux amplitude $\hat{\phi}_{\rm rf}$ is at its peak (0.23), zero (0.0), and negative maximum (-0.23)during a beat period. Figure 5(e) shows a cut through the $\delta_I = 0$ plane, plotting H as a function of δ_R at various rf flux values. In Fig. 5(f) a blow-up of the dashed region is shown that traces the minimum and maximum of H as the rf flux envelope evolves with time. Note that the state transition occurs at an rf flux amplitude of 0.22 for this frequency. When rf flux is zero, the Hamiltonian H is symmetric around the origin, and has a local minimum (stable point) centered at the origin. As the rf flux increases, the $H(\delta_R)$ curve tilts so that the peak located in the positive region of δ_R decreases and moves towards the origin; gradually meeting the dip which moves away from the origin along the δ_R axis. At the same time another peak rises up. As the rf flux value reaches 0.23, the lower peak and the dip between the two peaks disappear. The system then has to transition to another stable state located at the higher peak in the negative δ_R region. At an rf flux of -0.23, H tilts to the other side [Fig. 5(c)].

Because of the high value of Q, the system's transition trajectory from one stable state to another follows the constant contour lines of the Hamiltonian surfaces in a spiral manner.



FIG. 5. The calculated Hamiltonian of a single rf SQUID as a function of δ_R and δ_I for rf flux amplitudes of (a) 0.23, (b) 0.0, and (c) -0.23. (d) The color map of the calculated Hamiltonian as a function of δ_R and δ_I for rf flux amplitude of 0.23, with contours from -1 to -0.5 with a step of 0.05. (e) The calculated Hamiltonian as a function of δ_R when $\delta_I = 0$ with different values of rf flux. (f) A zoom-in plot of the dashed box in (e). The transition rf flux value to bistability is around 0.22. All assume a center frequency of 17.35 GHz.

Figure 5(d) shows the contour lines (from -1 to -0.5 with a step of 0.05) on top of the Hamiltonian color map at $\hat{\phi}_{rf} = 0.23$.

We can find the trajectory of $\hat{\delta}(t)$ for $\phi_{dc} = 0$ by solving Eq. (8) to obtain δ_R and δ_I during a beat period as $\hat{\phi}_{rf}$ changes. Again, we look at the solutions for a center frequency of 17.35 GHz at -65 dBm input tone power. The time trajectory of the phase envelope $\hat{\delta}$ in the δ_R - δ_I plane during the beat period as calculated by the dynamical model is shown in Fig. 6(a). Compare this with Figs. 6(b) and 6(c) which present the $\hat{\delta}$ trajectories extracted from $\delta(t)$ in the full nonlinear numerical calculation and the steady-state model, respectively. Figures 6(a) and 6(b) are almost identical to each other, serving to validate the dynamical model. In the trajectory plots Figs. 6(a) and 6(b) we see four colored in-spiraling orbits centered around four corresponding dense regions (red and black dense regions are close to each other near the origin); the dense regions denote the steady-state solutions right after a state jump. We can clearly see these four states in the steady-state trajectory [Fig. 6(c)] labeled as A, B, C, and D. The blue dense region in Figs. 6(a) and 6(b) is the solution at the beginning of a beat period, corresponding to state A. As the rf flux amplitude during a beat period reduces below ϕ_{hl} , the high-amplitude state has to jump to state B (red). For the steady-state solution [Fig. 6(c)], the system oscillates in the high-amplitude branch following the blue curve, then directly jumps to state B (red dot). In numerical simulation of Eq. (2) and the dynamical model Eqs. (10a) and (10b) though, the system goes through several orbits before settling down at the low-amplitude stable state B (red dense region) near the origin in the δ plane. It follows from Eqs. (10a) and (10b) that the area in phase enclosed by the orbit decreases exponentially at a rate 2/Q during approach to the equilibrium point. The boundary between the two colors denotes the time when the system starts to jump to another state.

The in-spiraling orbits during a transition are predicted by the Hamiltonian analysis. The shape of the trajectory before



FIG. 6. The time elapsed trajectories for $\hat{\delta}(t)$ for one beat period calculated by (a) the dynamical model, (b) the numerical simulation, and (c) the steady-state model. The inset of (c) zooms in on the trajectory around the origin by five times. (d) $\delta(t)$ calculated from the dynamical model, and (e) is a zoom-in of the dashed box in (d) showing the ringing behavior.

jumping to state A matches the contour lines in Fig. 5(d), except that the trajectory is not symmetric about δ_I axis due to the losses (parametrized by Q) which is not included in the Hamiltonian. The number of trajectory orbits during the transition illustrates the relaxation time of a state jump. The relaxation time also depends on the losses.

Figure 6(d) displays the $\delta(t)$ calculated by the dynamical model; Fig. 6(e) is a zoom-in for the selected region near a state jump. The colors match the colored curves in the trajectory plots Figs. 6(a) to 6(c). There are very clear ringing features during a jump, which is a reflection of damped spiral orbits. The ringing feature oscillates at a frequency of around 1.5 GHz, and can cause sidebands in the IM spectrum.

IV. DISCUSSION

Three models for IM generation in rf-SQUIDs have been discussed. The solutions to the full numerical nonlinear model contain the most complete information for the response of rf-SQUIDs to two-tone excitation, yet gives little insight into the underlying physics. The steady-state analytical model greatly simplifies the second order nonlinear differential equation to three coupled algebraic equations, and sheds light on the origin of the unique IM features-the state jumps during a beat period cause an abrupt increase in IM products. While it predicts the same level of IM generation as calculated by numerical simulation (Fig. 3), the steady-state model lacks the dynamics accompanying each state jump, which can be understood using the nonlinear dynamical model. This model reduces the full nonlinear equation to a complex first order differential equation, and allows for construction of a Hamiltonian for the SQUID. The topology of the Hamiltonian surfaces evolves continuously as the envelope of the drive signal changes. The topology determines the form of the trajectories $\hat{\delta}(t)$ to be spirals during transitions as the SQUID switches from one stable state to another, resulting in ringing features in $\delta(t)$.

The models all include dc flux as a variable that affects the response of the SQUID. In this paper we focus on the zero dc flux case. Varying the dc flux value would modify the relationship between the envelope of δ and the envelope of ϕ_{rf} [zero flux case shown in Fig. 4(a)], but would preserve bistability and thus the discontinuous jumps during a beat period. In the future we plan to explore the effect of nonzero dc flux on IM generation.

We also note that utilizing two equal-amplitude tone inputs always results in the rf flux envelope passing through zero during the beat period. Thus the IM products of the SQUID are independent of the system's history, even in the bistable regime. As long as the rf flux envelope peak (determined by tone power) exceeds the transition point ϕ_{lh} , the SQUID will experience four discontinuous jumps during a beat period. However, if the two tones have different amplitudes, so that the minimum value of the envelope is higher than ϕ_{hl} , the amplitude of the phase envelope depends on the direction of tone power sweep. In an upward sweep the phase amplitude $\hat{\delta}$ resides in the low-amplitude branch during the whole beat period until the tone power increases to the point that the rf flux envelope peak exceeds ϕ_{lh} ; δ will then keep oscillating in the high-amplitude branch during a beat period. In a downward tone power scan though, δ would modulate with the beating rf flux in the high-amplitude branch until the peak drops below ϕ_{hl} . The IM amplification experiment of an 11 × 11 SQUID array metamaterial, where the power amplitude of one tone is always 20 dB higher than the other, shows significantly more hysteresis in rf power scanning than the equal-amplitude IM case. The lack of discontinuous jumps during a beat period in the hysteretic IM amplification process brings in new phenomena worth investigating in the future.

V. CONCLUSION

We have shown that the rf-SQUID meta-atoms and metamaterials have a rich nonlinear spectrum due to the nonlinearity of the Josephson junctions. Experiment, numerical simulation, and analytic models all show a sharp onset, followed by a dip, in the third order IM output. rf-SQUID array metamaterials display behaviors that are similar to those of single rf-SQUID meta-atoms. The sharp onset of IM generation comes from a series of asymmetric jumps between two stable states of the rf-SQUID as the drive amplitude modulates during a beat period of the input signal. Each state jump creates a transient response appearing as ringing in the time domain. The time evolution of the junction gauge-invariant phase $\delta(t)$ can be explained by a dynamical model employing a Hamiltonian analysis with damping. Our analytical models can potentially be used to design SQUID metamaterials to generate either very high or very low IM products in response to multitone excitation. In addition, these models can also be applied to design other nonlinear systems employing Josephson junctions, such as the Josephson parametric amplifiers.

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- R. Vijay, M. H. Devoret, and I. Siddiqi, Invited review article: The Josephson bifurcation amplifier, Rev. Sci. Instrum. 80, 111101 (2009).
- [2] H. G. LeDuc, B. H. Eom, P. K. Day, and J. Zmuidzinas, A wideband, low-noise superconducting amplifier with high dynamic range, Nat. Phys. 8, 623 (2012).
- [3] O. Yaakobi, L. Friedland, C. Macklin, and I. Siddiqi, Parametric amplification in Josephson junction embedded transmission lines, Phys. Rev. B 87, 144301 (2013).
- [4] J. Mateu, J. C. Booth, C. Collado, and J. M. O'Callaghan, Intermodulation distortion in coupled-resonator filters with nonuniformly distributed nonlinear properties—use in HTS IMD compensation, IEEE Trans. Microwave Theory Tech. 55, 616 (2007).
- [5] M. Lapine, I. V. Shadrivov, and Y. S. Kivshar, *Colloquium*: Nonlinear metamaterials, Rev. Mod. Phys. 86, 1093 (2014).
- [6] I. V. Shadrivov, A. B. Kozyrev, D. W. van der Weide, and Y. S. Kivshar, Tunable transmission and harmonic generation in nonlinear metamaterials, Appl. Phys. Lett. 93, 161903 (2008).
- [7] K. D. Irwin, G. C. Hilton, L. R. Vale, and K. W. Lehnert, Amplification and squeezing of quantum noise with a tunable Josephson metamaterial, Nat. Phys. 4, 929 (2008).
- [8] C. Lee and C. Seo, Control scheme of harmonics and third-order intermodulation distortion with composite right/left-handed structure for linearity enhancement of power amplifier module, Microwave Opt. Technol. Lett. 55, 1497 (2013).
- [9] M. Gil, J. Bonache, J. Garcia-Garcia, J. Martel, and F. Martin, Composite right/left-handed metamaterial transmission lines based on complementary split-rings resonators and their applications to very wideband and compact filter design, IEEE Trans. Microwave Theory Tech. 55, 1296 (2007).
- [10] M. Gil, J. Bonache, and F. Martín, Metamaterial filters: A review, Metamaterials 2, 186 (2008).
- [11] C. M. Watts, C. C. Nadell, J. Montoya, S. Krishna, and W. J. Padilla, Frequency-division-multiplexed single-pixel imaging with metamaterials, Optica 3, 133 (2016).
- [12] S. Lim, C. Caloz, and T. Itoh, Metamaterial-based electronically controlled transmission-line structure as a novel leaky-wave antenna with tunable radiation angle and beamwidth, IEEE Trans. Microwave Theory Tech. 53, 161 (2005).
- [13] R. W. Ziolkowski and A. Erentok, Metamaterial-based efficient electrically small antennas, IEEE Trans. Antennas Propag. 54, 2113 (2006).
- [14] Y. Dong, H. Toyao, and T. Itoh, Design and characterization of miniaturized patch antennas loaded with complementary splitring resonators, IEEE Trans. Antennas Propag. 60, 772 (2012).
- [15] J. C. Pedro and N. B. Carvalho, *Intermodulation Distortion in Microwave and Wireless Circuits* (Artech House, Norwood, MA, 2002).
- [16] Z. Y. Shen, *High-Temperature Superconducting Microwave Circuits*, Artech House Antennas and Propagation Library (Artech House, Norwood, MA, 1994).

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- [17] M. T. Abuelma'atti, Harmonic and intermodulation performance of Josephson junctions, Int. J. Infrared Millimeter Waves 14, 1299 (1993).
- [18] B. A. Willemsen, T. Dahm, and D. J. Scalapino, Microwave intermodulation in thin film high-T_c superconducting microstrip hairpin resonators: Experiment and theory, Appl. Phys. Lett. 71, 3898 (1997).
- [19] T. Dahm and D. J. Scalapino, Intermodulation and quality factor of high-T_c superconducting microstrip structures, J. Appl. Phys. 82, 464 (1997).
- [20] J. McDonald, J. R. Clem, and D. E. Oates, Critical-state model for intermodulation distortion in a superconducting microwave resonator, J. Appl. Phys. 83, 5307 (1998).
- [21] R. B. Hammond, E. R. Soares, Balam A. Willemsen, T. Dahm, D. J. Scalapino, and J. R. Schrieffer, Intrinsic limits on the Q and intermodulation of low power high temperature superconducting microstrip resonators, J. Appl. Phys. 84, 5662 (1998).
- [22] G. Benz, T. A. Scherer, M. Neuhaus, and W. Jutzi, Quality factor and intermodulation product of superconducting coplanar wave guides with slots in a DC magnetic field, IEEE Trans. Appl. Supercond. 9, 3046 (1999).
- [23] S. K. Remillard, H. ren Yi, and A. Abdelmonem, Threetone intermodulation distortion generated by superconducting bandpass filters, IEEE Trans. Appl. Supercond. 13, 3797 (2003).
- [24] J. Mateu, C. Collado, O. Menéndez, and J. M. O'Callaghan, A general approach for the calculation of intermodulation distortion in cavities with superconducting endplates, Appl. Phys. Lett. 82, 97 (2003).
- [25] J. Mateu, C. Collado, N. Orloff, J. C. Booth, E. Rocas, A. Padilla, and J. M. O'Callaghan, Third-order intermodulation distortion and harmonic generation in mismatched weakly nonlinear transmission lines, IEEE Trans. Microwave Theory Tech. 57, 10 (2009).
- [26] E. Rocas, C. Collado, N. D. Orloff, J. Mateu, A. Padilla, J. M. O'Callaghan, and J. C. Booth, Passive intermodulation due to self-heating in printed transmission lines, IEEE Trans. Microwave Theory Tech. 59, 311 (2011).
- [27] E. A. Tholén, A. Ergül, D. Schaeffer, and D. B. Haviland, Gain, noise and intermodulation in a nonlinear superconducting resonator, EPJ Quantum Technol. 1, 5 (2014).
- [28] D. E. Oates, H. Xin, G. Dresselhaus, and M. S. Dresselhaus, Intermodulation distortion and Josephson vortices in YBCO bicrystal grain boundaries, IEEE Trans. Appl. Supercond. 11, 2804 (2001).
- [29] D. E. Oates, S. H. Park, M. A. Hein, P. J. Hirst, and R. G. Humphreys, Intermodulation distortion and thirdharmonic generation in YBCO films of varying oxygen content, IEEE Trans. Appl. Supercond. 13, 311 (2003).
- [30] A. P. Zhuravel, A. V. Ustinov, D. Abraimov, and S. M. Anlage, Imaging local sources of intermodulation in superconducting microwave devices, IEEE Trans. Appl. Supercond. 13, 340 (2003).

- [31] H. Xin, D. E. Oates, G. Dresselhaus, and M. S. Dresselhaus, Third-order intermodulation distortion in $YBa_2Cu_3O_{7-\delta}$ grain boundaries, Phys. Rev. B **65**, 214533 (2002).
- [32] B. A. Willemsen, K. E. Kihlstrom, T. Dahm, D. J. Scalapino, B. Gowe, D. A. Bonn, and W. N. Hardy, Microwave loss and intermodulation in Tl₂Ba₂CaCu₂O_y thin films, Phys. Rev. B 58, 6650 (1998).
- [33] L. Hao, J. Gallop, A. Purnell, L. Cohen, and S. Thiess, Nonlinear microwave response of HTS thin films: A comparison of intermodulation and conventional measurements, IEEE Trans. Appl. Supercond. 11, 3411 (2001).
- [34] G. Lamura, A. J. Purnell, L. F. Cohen, A. Andreone, F. Chiarella, E. Di Gennaro, R. Vaglio, L. Hao, and J. Gallop, Microwave intermodulation distortion of MgB₂ thin films, Appl. Phys. Lett. 82, 4525 (2003).
- [35] A V Velichko, Origin of the deviation of intermodulation distortion in high-T_c thin films from the classical 3:1 scaling, Supercond. Sci. Technol. 17, 1 (2004).
- [36] D. E. Oates, S. H. Park, D. Agassi, G. Koren, and K. Irgmaier, Temperature dependence of intermodulation distortion in YBCO: understanding nonlinearity, IEEE Trans. Appl. Supercond. 15, 3589 (2005).
- [37] D. E. Oates, Y. D. Agassi, and B. H. Moeckly, Intermodulation distortion and nonlinearity in MgB₂: Experiment and theory, IEEE Trans. Appl. Supercond. 17, 2871 (2007).
- [38] H. W. Jang, K. J. Choi, C. M. Folkman, D. E. Oates, and C. B. Eom, Intermodulation distortion in epitaxial Y-Ba-Cu-O thick films and multilayers, IEEE Trans. Appl. Supercond. 19, 2855 (2009).
- [39] Y. D. Agassi, D. E. Oates, and B. H. Moeckly, Evidence for non-s-wave symmetry of the π gap in MgB₂ from intermodulation distortion measurements, Phys. Rev. B **80**, 174522 (2009).
- [40] E. K. Pease, B. J. Dober, and S. K. Remillard, Synchronous measurement of even and odd order intermodulation distortion at the resonant frequency of a superconducting resonator, Rev. Sci. Instrum. 81, 024701 (2010).
- [41] Y. D. Agassi and D. E. Oates, Intermodulation distortion and surface resistance in impurity-doped YBCO and MgB₂, Physica C 506, 119 (2014).
- [42] B. Abdo, O. Suchoi, E. Segev, O. Shtempluck, M. Blencowe, and E. Buks, Intermodulation and parametric amplification in a superconducting stripline resonator integrated with a dc-SQUID, Europhys. Lett. 85, 68001 (2009).
- [43] B. Abdo, E. Segev, O. Shtempluck, and E. Buks, Intermodulation gain in nonlinear NbN superconducting microwave resonators, Appl. Phys. Lett. 88, 022508 (2006).
- [44] T. Dahm and D. J. Scalapino, Theory of microwave intermodulation in a high-T_c superconducting microstrip resonator, Appl. Phys. Lett. 69, 4248 (1996).
- [45] T. C. L. G. Sollner, J. P. Sage, and D. E. Oates, Microwave intermodulation products and excess critical current in YBa₂Cu₃O_{7-x} Josephson junctions, Appl. Phys. Lett. 68, 1003 (1996).
- [46] T. Dahm and D. J. Scalapino, Theory of intermodulation in a superconducting microstrip resonator, J. Appl. Phys. 81, 2002 (1997).
- [47] B. A. Willemsen, K. E. Kihlstrom, and T. Dahm, Unusual power dependence of two-tone intermodulation in high-T_c superconducting microwave resonators, Appl. Phys. Lett. 74, 753 (1999).

- [48] T. Dahm, D. J. Scalapino, and B. A. Willemsen, Phenomenological theory of intermodulation in HTS resonators and filters, J. Supercond. 12, 339 (1999).
- [49] T. Dahm, D. J. Scalapino, and B. A. Willemsen, Microwave intermodulation of a superconducting disk resonator, J. Appl. Phys. 86, 4055 (1999).
- [50] W. Hu, A. S. Thanawalla, B. J. Feenstra, F. C. Wellstood, and S. M. Anlage, Imaging of microwave intermodulation fields in a superconducting microstrip resonator, Appl. Phys. Lett. 75, 2824 (1999).
- [51] E. A. Vopilkin, A. E. Parafin, and A. N. Reznik, Intermodulation in a microwave resonator with a high-temperature superconductor, Tech. Phys. 45, 214 (2000).
- [52] C. Hutter, D. Platz, E. A. Tholén, T. H. Hansson, and D. B. Haviland, Reconstructing Nonlinearities with Intermodulation Spectroscopy, Phys. Rev. Lett. 104, 050801 (2010).
- [53] S. M. Anlage, The physics and applications of superconducting metamaterials, J. Opt. 13, 024001 (2011).
- [54] P. Jung, A. V Ustinov, and S. M Anlage, Progress in superconducting metamaterials, Supercond. Sci. Technol. 27, 073001 (2014).
- [55] P. Jung, S. Butz, S. V. Shitov, and A. V. Ustinov, Low-loss tunable metamaterials using superconducting circuits with Josephson junctions, Appl. Phys. Lett. **102**, 062601 (2013).
- [56] S. Butz, P. Jung, L. V. Filippenko, V. P. Koshelets, and A. V. Ustinov, A one-dimensional tunable magnetic metamaterial, Opt. Express 21, 22540 (2013).
- [57] M. Trepanier, D. Zhang, O. Mukhanov, and S. M. Anlage, Realization and Modeling of Metamaterials Made of rf Superconducting Quantum-Interference Devices, Phys. Rev. X 3, 041029 (2013).
- [58] D. Zhang, M. Trepanier, O. Mukhanov, and S. M. Anlage, Tunable Broadband Transparency of Macroscopic Quantum Superconducting Metamaterials, Phys. Rev. X 5, 041045 (2015).
- [59] O. Mukhanov, G. Prokopenko, and R. Romanofsky, Quantum sensitivity: Superconducting quantum interference filter-based microwave receivers, IEEE Microwave Mag. 15, 57 (2014).
- [60] O. A. Mukhanov, D. Kirichenko, I. V. Vernik, T. V. Filippov, A. Kirichenko, R. Webber, V. Dotsenko, A. Talalaevskii, J. C. Tang, A. Sahu, P. Shevchenko, R. Miller, S. B. Kaplan, S. Sarwana, and D. Gupta, Superconductor digital-RF receiver systems, IEICE Trans. Electron. E91-C, 306 (2008).
- [61] C. G. Du, H. Y. Chen, and S. Q. Li, Quantum left-handed metamaterial from superconducting quantum-interference devices, Phys. Rev. B 74, 113105 (2006).
- [62] N. Lazarides and G. P. Tsironis, RF superconducting quantum interference device metamaterials, Appl. Phys. Lett. 90, 163501 (2007).
- [63] A. I. Maimistov and I. R. Gabitov, Nonlinear response of a thin metamaterial film containing Josephson junctions, Opt. Commun. 283, 1633 (2010).
- [64] N. Lazarides and G. P. Tsironis, Multistability and selforganization in disordered SQUID metamaterials, Supercond. Sci. Technol. 26, 084006 (2013).
- [65] P. Jung, S. Butz, M. Marthaler, M. V. Fistul, J. Leppäkangas, V. P. Koshelets, and A. V. Ustinov, Multistability and switching in a superconducting metamaterial, Nat. Commun. 5, 3730 (2014).
- [66] G. P. Tsironis, N. Lazarides, and I. Margaris, Wide-band tuneability, nonlinear transmission, and dynamic multistability in SQUID metamaterials, Appl. Phys. A 117, 579 (2014).

- [67] P. Jung, Nonlinear effects in superconducting quantum interference meta-atoms, Ph.D. thesis, Karlsruher Institut für Technologie (KIT), 2014, http://www.ksp.kit.edu/ download/1000043835.
- [68] J. Hizanidis, N. Lazarides, and G. P. Tsironis, Robust chimera states in SQUID metamaterials with local interactions, Phys. Rev. E 94, 032219 (2016).
- [69] D. Zhang, Radio frequency superconducting quantum interference device meta-atoms and metamaterials: Experiment, theory,

and analysis, Ph.D. thesis, University of Maryland, College Park, 2016, http://drum.lib.umd.edu/handle/1903/18805.

- [70] B. Chesca, Theory of RF SQUIDs operating in the presence of large thermal fluctations, J. Low Temp. Phys. 110, 963 (1998).
- [71] K. K. Likharev, *Dynamics of Josephson Junctions and Circuits* (Gordon and Breach, New York, 1986).
- [72] Whiteley Research, http://www.wrcad.com/.
- [73] S. Doyle, Lumped element kinetic inductance detectors, Ph.D. thesis, University of Cardiff, Cardiff, UK, 2008.